

# Material Time Constant Characterizing the Nonlinear Viscoelasticity of Entangled Polymeric Systems

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**ABSTRACT:** For concentrated polystyrene solutions, the effect of varying strain on the relaxation modulus can be described with the tube-model theory of Doi and Edwards at times longer than a certain characteristic time  $\tau_k$  determined for each sample. The characteristic time is proportional to the second power of the number of entanglements per molecule and has been conjectured to define the complete equilibration of the fluctuation of the primitive path length. Here, we see that  $\tau_k$  is about 4.5 times as large as the configurational relaxation time of an isolated (unentangled) polymer molecule in a hypothetical viscous medium that exerts the same frictional force to polymer segments as the polymer solution does. We also see that the same holds true for polystyrene solutions of relatively low concentrations if the entanglement molecular weight  $M_e$  is assumed to be proportional to the  $-1.4$  power of the concentration in this case.

## Introduction

In 1978 Doi and Edwards proposed a novel molecular theory on the viscoelastic properties of entangled polymeric systems.<sup>1</sup> The theory has been proved to be well in accord with many experimental observations, especially on the nonlinear viscoelasticity.<sup>2-4</sup> The theory is based on the tube model of de Gennes.<sup>5</sup> In this model each polymer chain is allowed to move in a tubelike region that is bounded by surrounding polymer chains. This constraint on the motion of the polymer does not affect the rate of change of the primitive path length. The equilibration time of the contour length of the primitive path or chain  $T_{eq}$  is proportional to the second power of the number of entanglement points per chain  $N_e$ . The quantity  $T_{eq}$  is the same as the equilibration time of the large-scale configuration of a polymer molecule dissolved in a hypothetical unentangled viscous medium in which the viscous force exerted to polymer segments is the same as that exerted in the tubelike region. We call this time constant the configurational relaxation time for short and assign a notation  $\tau_c$  for it. On the other hand, the large-scale orientation of the chain in the tube model changes very slowly as the chain creeps out of the tubelike region through reptating motion. Thus the time constant characterizing the change of orientation of the chain is that characterizing the disengagement of the chain from the tubelike region  $T_d$ . This is proportional to  $N_e^3$  and is usually much larger than  $T_{eq}$  when  $N_e$  is large. According to a recent theory by Doi,  $T_d$  should be proportional to  $N_e^{3.5}$  over a wide range of  $N_e$  of practical importance.<sup>6</sup> The Doi-Edwards theory leads to a rather simple expression for stresses at times sufficiently longer than  $T_{eq}$  in the stress relaxation process or for those in any flow histories of rates of strain much smaller than  $T_{eq}^{-1}$ .

On the other hand, the shear relaxation modulus at large deformations had extensively been studied for concentrated solutions of polystyrenes with narrow molecular weight distributions.<sup>7,8</sup> It was observed that the relaxation modulus  $G(t, \gamma)$  could be factored into two functions, one of time  $t$  and the other of magnitude of shear  $\gamma$ , as

$$G(t, \gamma) = G(t)h(\gamma) \quad t > \tau_k \quad (1)$$

at times longer than a certain critical value  $\tau_k$  determined for each material. The strain-dependent function  $h(\gamma)$  was common to many systems of various molecular weights and concentrations.<sup>8</sup> It turned out to have the same strain dependence as derived by Doi and Edwards.<sup>1,2</sup> Then the empirical quantity  $\tau_k$  was suspected to represent a time "sufficiently longer than  $T_{eq}$ ." The idea is supported by

Table I  
 $\tau_1^0$  and  $\tau_k$  for Moderately Concentrated Polystyrene Solutions

$M_w/10^4$	$c/(10^{-2} \text{ g cm}^{-3})$	$\tau_k/\text{s}$	$\tau_1^0/\text{s}$
448	5	20 <sup>a</sup>	20
	6	22	54
	7	25	83
	8	30	122
842	2	6.5 <sup>a</sup>	6.5
	3	30	42
	4	40	99
	5	40	160
	6	45	380

<sup>a</sup> $G(t, \gamma)$  is factorizable only at  $t \geq \tau_1^0$ .

some observations<sup>9</sup> that the viscoelastic behavior is in conflict with the prediction of the theory when the rate of shear is higher than  $\tau_k^{-1}$ . In addition, the quantity  $\tau_k$  has been proved to be proportional to  $N_e^2$  in the range of high concentrations,<sup>10</sup> where the critical molecular weight corresponding to the entanglement spacing is inversely proportional to concentration.

The purpose of the present study is to examine the nature of  $\tau_k$  in more detail and to see if it is really related to the theoretical quantity  $T_{eq}$ . For this purpose, we measure the concentration dependence of  $\tau_k$  in moderately concentrated solutions, in which the critical molecular weight is affected more strongly by the concentration than in highly concentrated solutions. We also evaluate the configuration relaxation time  $\tau_c$  in a hypothetical viscous medium and compare it with the value of  $\tau_k$ .

## Materials and Apparatus

Measurements were performed on polystyrene solutions in chlorinated biphenyl, Aroclor 1248. Two polystyrene samples were supplied from Toyo Soda Manufacturing Co. According to the data given by the supplier, the weight-average molecular weights  $M_w$  were  $4.48 \times 10^6$  and  $8.42 \times 10^6$ , respectively, and the ratios of  $M_w$  to the number-average molecular weight  $M_n$  were 1.14 and 1.17, respectively. The concentration ranged from 0.02 to 0.08 g cm<sup>-3</sup> at 30 °C as shown in Table I.

The shear relaxation modulus  $G(t, \gamma)$  was measured with a cone-and-plate relaxometer.<sup>11</sup> The sample was held in the gap between the cone and the plate, and the plate was rotated instantaneously through a certain angle. The magnitude of shear  $\gamma$  was evaluated from the rotation angle. The shear stress was evaluated from the torque exerted on the cone. The quantity  $G(t, \gamma)$  was obtained as the ratio of the shear stress to  $\gamma$ . For most of the samples, the measurements were performed over the range of  $\gamma$  from 0.5 to 6. For the remaining samples, measurements

were performed up to the  $\gamma$  value of 20. All the measurements were performed at 30 °C.

### Relevant Quantities and Equations

The maximum relaxation time  $\tau_1^0$  for linear relaxation modulus  $G(t)$  was evaluated from the slope of the asymptotic straight line at long times on a graph of  $\log G(t)$  plotted against  $t$ .<sup>12</sup> The characteristic time  $\tau_k$  was defined as the time at which the relaxation modulus  $G(t, \gamma)$  begins to be factored as shown in eq 1. The actual procedure of estimating  $\tau_k$  and  $h(\gamma)$  from  $G(t, \gamma)$  will be shown later (see Figure 2).

For highly concentrated polystyrene solutions, we have seen that

$$\tau_1^0 / \tau_k \propto (M/M_e)^{1.5} \quad (2)$$

where  $M_e$  is the molecular weight of the chain between entanglement points.<sup>10</sup> This result implies that  $\tau_k$  is proportional to  $(M/M_e)^2$  (apart from an extra factor of concentration included in the segmental friction coefficient) since  $\tau_1^0$  is proportional to  $(M/M_e)^{3.5}$ . For evaluation of  $M_e$  in eq 2, the following relation for concentrated solutions<sup>13</sup> is employed:

$$cM_e = 2 \times 10^4 \text{ g cm}^{-3} \quad (3)$$

The values of  $M_e$  from various literature sources may be within 20% of the value from eq 3. A different choice for the value on the right-hand side will not much affect the results shown later. For moderately concentrated solutions, the quantity  $M_e$  is believed to vary as

$$c^\alpha M_e = \text{constant} \quad \alpha > 1 \quad (4)$$

Onogi et al. showed that  $\alpha$  varies from 1.4 to 2.0, depending on the combination of polymer and solvent.<sup>14</sup> Doi asserts that  $\alpha$  ranges from 2 to 1 as the concentration increases.<sup>15</sup> The recent blob theory gives  $\alpha = 1.25$  when the excluded volume effect is large.<sup>16</sup> If eq 2 is to hold good in the range of concentration of the present measurements, the ratio  $\tau_1^0 / \tau_k$  should be proportional to  $c^{1.5\alpha}$  instead of  $c^{1.5}$ .

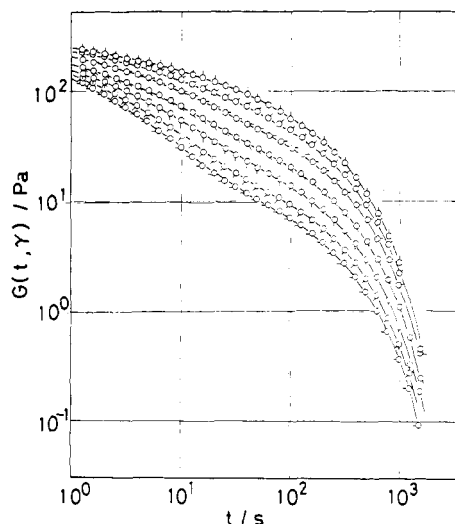
In evaluating the configurational relaxation time  $\tau_c$  in a hypothetical viscous medium, we assume that the frictional resistance of the polymer segments in the tubelike region is equal to that in a solution of a polymer with a molecular weight lower than the entanglement molecular weight at that concentration. We employ the spring-bead model, or the Rouse model,<sup>17</sup> for evaluation of  $\tau_c$  and assign a notation  $\tau_{cR}$  to indicate the model. For an unentangled polymer molecule in a viscous medium, the configurational (or vector mode) relaxation time  $\tau_{cR}$  is twice as large as the maximum viscoelastic (or tensor mode) relaxation time  $\tau_R$ .<sup>18</sup> The Rouse theory gives

$$\tau_R = \frac{6M\eta^0}{\pi^2 cRT} \quad (\text{not entangled}) \quad (5)$$

where  $\eta^0$  is the viscosity of the polymer solution,  $R$  is the gas constant, and  $T$  is the absolute temperature. Equation 5 is in accord with experimental results for concentrated polymer solutions of low molecular weights, for which the viscosity is proportional to the molecular weight.<sup>18</sup> When the molecular weight is higher than about  $2M_e$ , the viscosity is proportional to  $M^{3.5}$ . We assume then that the viscosity is enhanced by a factor  $(M/2M_e)^{2.5}$  due to the effect of entanglement<sup>19</sup> and obtain the expression

$$\eta_H = \eta^0 (2M_e/M)^{2.5} \quad (6)$$

for the viscosity of the hypothetical viscous medium that exerts the same frictional force to polymer segments as the



**Figure 1.** Relaxation modulus  $G(t, \gamma)$  for polystyrene solution of chlorinated biphenyl at 30 °C. The molecular weight of the polymer is  $8.42 \times 10^6$  and the concentration is  $0.06 \text{ g cm}^{-3}$ . Magnitudes of shear  $\gamma$  are <0.57, 1.25, 2.06, 3.04, 4.0, 5.3, and 6.1 from top to bottom.

entangled polymeric system does. The configurational relaxation time of an isolated polymer molecule in the hypothetical medium is given by

$$\tau_{cR} = \frac{12M\eta_H}{\pi^2 cRT} \quad (7)$$

This can be evaluated from the data of  $\eta^0$ . The viscosity is evaluated from the linear relaxation modulus  $G(t)$  through the relation<sup>20</sup>

$$\eta^0 = \int_0^\infty G(t) dt \quad (8)$$

### Results and Discussion

**Relaxation Modulus for Moderately Concentrated Solutions.** The relaxation modulus  $G(t, \gamma)$  for a  $0.06 \text{ g cm}^{-3}$  solution of the polystyrene of  $M_w = 8.42 \times 10^6$  is shown in Figure 1 as an example. The curve at the top represents the results obtained for  $\gamma \leq 0.57$  and so the linear relaxation modulus  $G(t)$ . As  $\gamma$  increases, the relaxation modulus  $G(t, \gamma)$  decreases and the shape of the curve changes;  $G(t, \gamma)$  for large  $\gamma$  markedly decreases in two different ranges of times, indicating the existence of two mechanisms of stress relaxation.

Each curve corresponding to  $\gamma \geq 1.25$  in Figure 1 is shifted vertically so that it is superposed on the curve for  $G(t)$  at  $t \approx \tau_1^0$ . The result is shown in Figure 2. The amount of shift here is denoted by  $-\log h(\gamma)$ . Obviously, the quantity  $G(t, \gamma)$  can be factored into two functions  $G(t)$  and  $h(\gamma)$  as in eq 1 at times longer than a certain time  $\tau_k$ , 40 s in this case. Results similar to those shown in Figures 1 and 2 are obtained also for other solutions. The results for  $\tau_1^0$  and  $\tau_k$  are shown in Table I and the results for  $h(\gamma)$  are shown in Figure 3.

The circles in Figure 3 represent the values of  $h(\gamma)$  obtained experimentally. Filled circles are for  $M_w = 8.42 \times 10^6$  and open circles for  $M_w = 4.48 \times 10^6$ , and various directions of the pips represent concentrations. At the lowest concentration studied for each molecular weight, the stress for  $\gamma < 1$  was too small to be measured and so the function  $h(\gamma)$  was not determined. One sees that the quantity  $h(\gamma)$  scarcely varies with molecular weight or concentration. The theoretical value of  $h(\gamma)$  due to the Doi-Edwards theory, represented by the solid curve, is in good agreement with the observed values over a wide range

Table II  
Conformational Relaxation Time  $\tau_{cR}$  and Related Quantities for Polystyrene Solutions

$M_w/10^4$	$c/(10^{-2} \text{ g cm}^{-3})$	$\eta^0/(\text{kPa s})$	$\tau_{cR}/\text{s}$	$\tau_k/\text{s}$	$\tau_1^0/\text{s}$	$\tau_k/\tau_{cR}$	ref
67	40	4940	34	165	1100	4.9	ref 10
95	20	28.8	1.3	6.0	18.4	4.6	ref 10
	30	925	10	40	285	4.0	ref 10
	40	27800	110	380	4200	3.5	ref 10
448	6	2.60	3.6	22	54	6.1	this work
	8	22.0	5.7	30	122	5.3	this work
842	4	2.98	9.3	40	99	4.3	this work
	6	23.6	12	45	380	3.8	this work

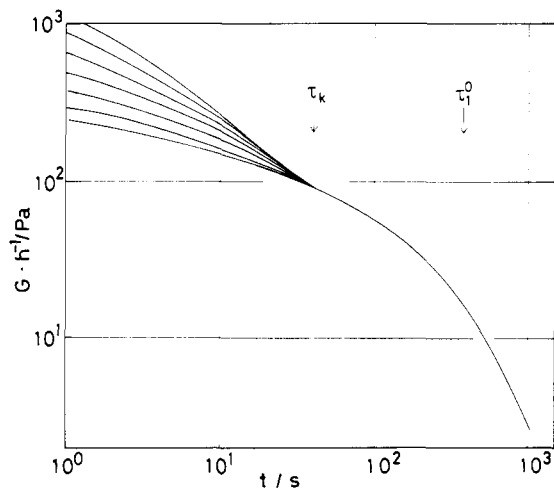


Figure 2. Reduced relaxation modulus  $G(t, \gamma)/h(\gamma)$  derived from Figure 1. Each curve for  $\gamma \geq 1.25$  in Figure 1 is shifted vertically by an amount  $-\log h(\gamma)$  so that it superposes on the top curve at  $t \approx \tau_1^0$ . Magnitudes of shear  $\gamma$  are 6.1, 5.3, 4.0, 3.04, 2.06, 1.25, and  $<0.57$  from top to bottom.

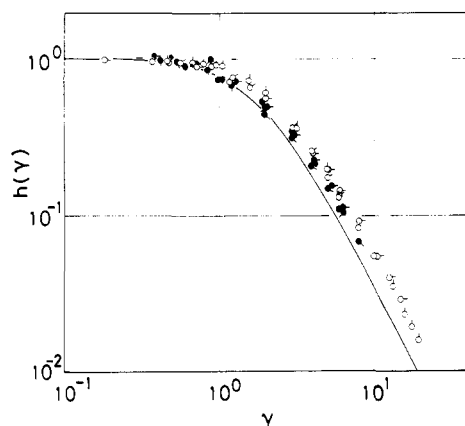


Figure 3.  $h(\gamma)$  determined from the relaxation modulus. Filled circles represent polystyrene of molecular weight  $8.42 \times 10^6$  and unfilled circles of  $4.48 \times 10^6$ . Directions of pips indicate concentrations as explained in the caption of Figure 4. The solid curve represents the theoretical value due to the Doi-Edwards theory.

of  $\gamma$ . (The curve is obtained without using the independent alignment assumption.<sup>1</sup>) Thus we may conclude that the strain dependence of the relaxation modulus at long times is well described with the Doi-Edwards theory even for solutions of relatively low concentrations.

**Concentration Dependence of  $\tau_k$ .** The ratio  $\tau_1^0/\tau_k$  is plotted against  $M/M_e$  in Figure 4. Here, the quantity  $M_e$  is evaluated with eq 3. The unfilled circles without pips represent the results for  $c \geq 0.20 \text{ g cm}^{-3}$  reported earlier.<sup>10</sup> The double circle represents the result<sup>21</sup> for  $c = 0.112 \text{ g cm}^{-3}$  and  $M_w = 3.0 \times 10^6$ . The circles with pips represent the present results. Evidently the values for  $c \geq 0.20 \text{ g cm}^{-3}$

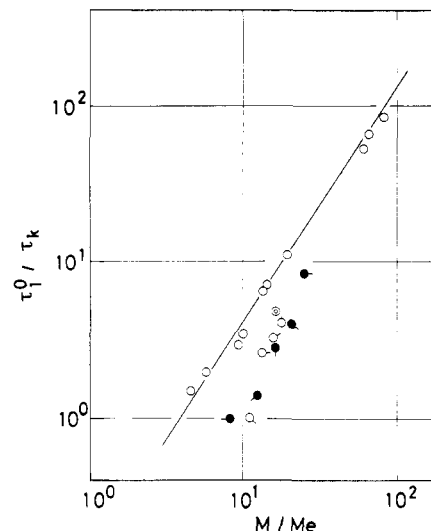


Figure 4.  $\tau_1^0/\tau_k$  for polystyrene solutions of various molecular weights  $M$  and concentrations  $c$ . The abscissa is the number of entanglements per molecule evaluated with the use of eq 3. Unfilled circles without pips represent results for  $c \geq 0.20 \text{ g cm}^{-3}$ ; the double circle represents  $M = 3.0 \times 10^6$  and  $c = 0.112 \text{ g cm}^{-3}$ ; filled circles represent  $M = 8.42 \times 10^6$  and unfilled circles with pips,  $M = 4.48 \times 10^6$ . Directions of pips indicate concentrations: pip up,  $0.08 \text{ g cm}^{-3}$ ; successive  $45^\circ$  rotations clockwise correspond to 0.07, 0.06, 0.05, 0.04, 0.03, and  $0.02 \text{ g cm}^{-3}$ . The solid line is drawn with slope 1.5.

can be approximated by a straight line drawn with the slope 1.5. On the other hand, the values for  $c \leq 0.112 \text{ g cm}^{-3}$  are much lower than those evaluated from the line.

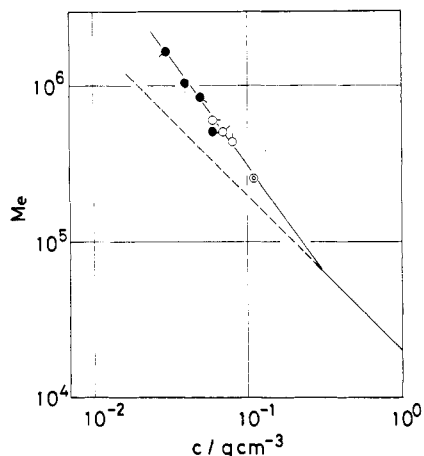
In view of eq 4, we may suppose that the deviation is due to the illegitimate use of eq 3 at relatively low concentrations. If this is the case, we may evaluate the correct values of  $M_e$  for moderate concentrations by assuming that all the points should lie on the solid line. The quantity  $M_e$  thus determined is approximately a function of concentration alone as seen in Figure 5: The points obtained for samples of various molecular weights support a single line when plotted against concentration. The straight line drawn through the data points has a slope  $-1.4$  and crosses the line representing eq 3 at  $c = 0.3 \text{ g cm}^{-3}$ . Thus we obtain

$$cM_e = 2 \times 10^4 \text{ g cm}^{-3} \quad c \geq 0.3 \text{ g cm}^{-3} \quad (9a)$$

$$c^{1.4}M_e = 1.23 \times 10^4 (\text{g cm}^{-3})^{1.4} \quad c < 0.3 \text{ g cm}^{-3} \quad (9b)$$

This result seems to be consistent with the experimental or theoretical results in the literature.<sup>14-16</sup> Thus the result for relatively dilute solutions may not be inconsistent with eq 2.

**Configurational Relaxation Time  $\tau_{cR}$ .** The viscosity  $\eta^0$  evaluated with eq 8 and the configurational relaxation time  $\tau_{cR}$  evaluated with eq 6 and 7 are shown for a few samples in Table II. The values of  $M_e$  used in eq 6 are obtained from eq 9. The ratio  $\tau_k/\tau_{cR}$ , through scattering over the range from 3.5 to 6.1, does not seem to vary



**Figure 5.** Concentration dependence of the entanglement molecular weight  $M_e$  determined from Figure 4 with the procedure given in text.

systematically with varying concentration or molecular weight. Therefore we may conclude that

$$\tau_k \approx 4.5\tau_{cR} \quad (10)$$

This result may be in good accord with the view that  $\tau_{cR}$  is equal to the equilibration time of the chain contour length  $T_{eq}$  and that  $\tau_k$  represents a measure of a time sufficiently longer than  $T_{eq}$ . Suppose that a certain considerable portion of the stress is associated with a relaxation time  $\tau_{cR}$  and the rest of the stress with a broad distribution of relaxation time over a wide range of time. The strength of the former portion of stress becomes about 1% of its full strength at  $t = 4.5\tau_{cR}$ . This is just the right magnitude for that portion to cease to be detectable from the rest of the stress.

The present evaluation of the configuration relaxation time is based on the assumption that the frictional force

exerted on the polymer segment in the tubelike region is equal to that in an unentangled solution with the same concentration. The result obtained above may indicate that the frictional force in the tubelike region may be estimated fairly well with the present assumption.

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## 300-MHz $^1\text{H}$ NMR and 25-MHz $^{13}\text{C}$ NMR Investigations of Sequence Distributions in Vinyl Alcohol-Vinyl Acetate Copolymers

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**ABSTRACT:** The microstructure of vinyl alcohol-vinyl acetate (VOH-VA) copolymers was studied by  $^{13}\text{C}$  and  $^1\text{H}$  NMR techniques. Sequence distributions could be obtained from the methine triads (VOH, VOH, VOH), (VOH, VOH, VA), (VA, VOH, VA), (VA, VA, VA), (VA, VA, VOH), and (VOH, VA, VOH) observed in the 300-MHz proton spectra of the copolymers. These sequence distributions were found to be in agreement with analogous sequence distributions calculated from methylene dyads and carbonyl triads in the  $^{13}\text{C}$  NMR spectra of these copolymers. Combination of the two NMR techniques provides a powerful method for gaining information on the microstructure of this important class of copolymers.

## 1. Introduction

Previous papers have demonstrated that high-resolution  $^1\text{H}$  NMR methods are extremely useful for microstructural analysis of ethylene-vinyl alcohol (E-VOH) and ethylene-vinyl acetate (E-VA) copolymers.<sup>1,2</sup> From 220-MHz  $^1\text{H}$  NMR spectra of E-VOH and E-VA copolymers, the compositional and configurational distributions of the comonomers could be readily determined. As an alternative,  $^{13}\text{C}$  NMR has been used for a detailed analysis of

E-VA and E-VOH copolymers.<sup>3,4</sup> Moritani and Fujiwara<sup>5</sup> have combined  $^1\text{H}$  and  $^{13}\text{C}$  NMR to study the compositional distributions of vinyl acetate-vinyl alcohol (VA-VOH) copolymers. Through studies of the three  $^{13}\text{C}$  NMR compositional methylene dyads, quantitative determination of sequence distributions in the copolymers has become possible. On the other hand, van Raaijen and van der Velden et al.<sup>6</sup> have mainly concentrated on the mixed configurational-compositional carbonyl triad, and quan-